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**(54) A PRE-ALLOY POWDER FOR  
 THE MANUFACTURE OF ALLOYED  
 SINTERED STEEL WORKPIECES**

(71) We, **GFE GESELLSCHAFT  
 FÜR ELECTROMETALLURGIE MBH** a  
 German Company of 4000 Düsseldorf 1,  
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 of Germany do hereby declare the  
 invention, for which we pray that a patent  
 may be granted to us, and the method by  
 which it is to be performed, to be  
 particularly described in and by the  
 following statement:—

The invention generally relates to a pre-  
 alloy powder for the manufacture of  
 alloyed sintered steel workpieces, in which  
 manufacture a ferro-alloy is first produced  
 from the alloy elements required in the  
 sintered steel workpieces together with iron  
 and carbon, this is pulverised and milled to  
 a pre-alloy powder, the pre-alloy powder is  
 mixed with ductile iron powder, and the  
 mixture is pressed and sintered.

The manufacture of tool steels and high  
 speed steels from ferro-alloys is relatively  
 new. So far as other steels have been  
 manufactured by powder metallurgy, one  
 has worked with fully alloyed materials  
 manufactured by the melting method and  
 subsequently converted by spraying into  
 the necessary powder form. These alloy  
 powders possess the complete composition  
 of the steel that is to be sintered, but have  
 the disadvantage of a considerable oxygen  
 content. The oxygen content affects the  
 mechanical properties of the finished  
 workpieces. Moreover very high pressures  
 are necessary for pressing, greater by a

factor of 2 than the pressure normal in iron  
 powder metallurgy. If one works with lower  
 pressures, the tensile strength values  
 achieved are insufficient. Steels which  
 contain manganese and chromium and/or  
 vanadium are not at all practicable to make  
 in the manner described. In fact it is very  
 difficult to avoid oxidation of the alloyed  
 chromium or manganese with the sintering  
 atmosphere used in practice. A reduction  
 of oxides introduced by these alloying  
 elements cannot be accomplished in  
 furnaces used for the sintering technique.  
 At least if one attempts to work with  
 manganese and chromium and/or  
 vanadium-additions, the tensile strengths  
 achieved by the known process are for this  
 reason inadequate.

According to the present invention a pre-  
 alloy powder for the manufacture of  
 alloyed sintered steel workpieces comprises  
 a pulverized ferro-alloy comprising  
 manganese and chromium or manganese  
 and vanadium in the form of complex  
 metallic carbides, with a grain size less than  
 10  $\mu\text{m}$ , having an oxygen content of less  
 than 0.2% and resistant to oxidation at  
 temperatures in the region of 1200°C.

Pressing forces normal in iron powder  
 metallurgy, are about 500 MN/m<sup>2</sup>.  
 Preferably the sintering temperature is up  
 to 1280°C.

Within the scope of the invention  
 complex metallic carbides signify carbides

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of at least two of the given elements and iron, mostly in the form of solid solutions.

The invention depends upon the surprising fact that a ferro-alloy consisting of the given complex metallic carbides, when pulverised, does not absorb oxygen, or at least does not do so to a troublesome extent. Therefore the pre-alloy powder, when a protective fluid is used in grinding to a grain-size below  $10\text{ }\mu\text{m}$ , preferably below  $5\text{ }\mu\text{m}$ , can without difficulty be limited to an oxygen content below 0.2%, preferably less than 0.15% even if it is milled extremely finely. The pre-alloy powder which is to be used for the manufacture of a sintered workpiece possesses a quite surprising resistance to oxidation, even at temperatures up to  $1200^{\circ}\text{C}$  and more. Difficulties caused by high oxide content of the powder which is to be pressed and sintered to form steel workpieces, and the influence on the tensile strength of the manufactured sintered steel workpieces are eliminated no longer occur. It can be accepted that the complex metallic carbides of manganese plus chromium, or of manganese plus vanadium, effect an additional protection against oxidation. This is also valid with extremely fine milling. It has been found that the alloy elements diffuse very readily during sintering, so that a very homogeneous distribution of the elements is achieved in the finished sintered steel workpiece which has a beneficial effect on the mechanical properties e.g. on tensile strength and hardenability. Examples of ferro-alloy powder and analyses of ferro-alloy powders which are particularly suitable for manufacturing sintered steel workpieces are in % by weight:—

20—25% Manganese  
20—25% Chromium  
4— 8% Carbon  
Balance iron

with impurities due to melting

30—35% Manganese  
35—45% Chromium  
5— 7% Carbon  
Balance iron

with impurities due to melting.

20—25% Manganese  
20—25% Chromium  
20—25% Molybdenum  
6— 8% Carbon  
Balance iron

with impurities due to melting.

20—25% Molybdenum  
20—25% Vanadium with or  
without Niobium  
20—25% Manganese  
Up to 7% Carbon  
Balance iron

with impurities due to melting.

In the following is illustrated the use of the pre-alloy powder of the invention in terms of examples of its performance.

#### EXAMPLE 1

In manufacturing a sintered steel workpiece which contains as alloy elements manganese plus chromium and also molybdenum, normal commercial iron powder is thoroughly mixed with a complex metallic carbide powder according to the invention in proportions of 96% to 4% and pressed as a workpiece e.g. a gearwheel, with a pressure of  $500\text{ MN/m}^2$ . The complex metallic carbide powder contains 21% Cr, 20.8% Mn, 23.1% Mn and 7.8% C, balance Fe.

The milling of the complex metallic carbides took place in an attritor to an FSSS (Fischer Sub-sieve sizes) grain size of  $3\text{ }\mu\text{m}$ . the oxygen content of the powder amounted to 0.16%.  $(\text{Fe, Mn, Cr})_3\text{C}_1$  and  $\beta\text{-Mo}_2\text{C}$  were identified in the carbide phases. Sintering took place at  $1250^{\circ}\text{C}$  in a normal sintering furnace, e.g., in a rocker bar heating furnace with a cracked ammonia atmosphere. A test during the sintering process proved that up to  $1200^{\circ}\text{C}$  there was no oxidation of the metallic carbide powder, which, beginning at  $1100^{\circ}\text{C}$ , dissolved easily and completely by  $1250^{\circ}\text{C}$ . in the iron powder.

#### Example 2

In manufacturing a sintered steel workpiece which contains the alloy elements manganese plus vanadium plus molybdenum, normal commercial iron powder is thoroughly mixed with a complex metallic carbide powder according to the invention in proportions of 97% to 3% and pressed to the desired workpiece with a pressure of  $500\text{ MN/m}^2$ . The complex metal carbide powder contained 21% Mn, 22% Mo and 21.4% V, also 7.9% C balance Fe.

The manufacture of the powder again took place by fine milling in an attritor. The FSSS grain size amounted to  $5\text{ }\mu\text{m}$ , with an oxygen content of 0.19%. As carbide phases were found:  $\text{VC—Mo}_2\text{C}$  solid solutions, and the  $\text{M}_3\text{C}_1$  type in which M is chiefly iron and manganese.

Sintering took place at  $1280^{\circ}\text{C}$  in a cracked ammonia atmosphere. Again with the complex iron alloy carbide powder used here no oxidation could be conformed up to  $1200^{\circ}\text{C}$ .

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**WHAT WE CLAIM IS:—**

1. A pre-alloy powder for the manufacture of alloyed sintered steel workpieces comprising a pulverized ferro-alloy comprising manganese and chromium or manganese and vanadium in the form of complex metallic carbides, with a grain size of less than 10  $\mu\text{m}$ , having an oxygen content of less than 0.2% and resistant to oxidation at temperatures in the region of 1200°C.

2. A pre-alloy powder as claimed in Claim 1, wherein the grain size is less than 5  $\mu\text{m}$ .

3. A pre-alloy powder as claimed in Claim 1 or Claim 2, wherein the oxygen content is less than 0.15%.

4. A pre-alloy powder as claimed in any preceding Claim, consisting of by weight:—

20—25% Manganese  
20—25% Chromium  
4—8% Carbon  
Balance iron

with impurities due to melting.

5. A pre-alloy powder as claimed in any one of Claims 1 to 3 consisting of by weight:—

30—35% Manganese  
35—45% Chromium

5—7% Carbon  
Balance iron

with impurities due to melting.

6. A pre-alloy powder as claimed in any one of Claims 1 to 3, consisting of by weight:—

20—25% Manganese  
20—25% Chromium  
20—25% Molybdenum  
6—8% Carbon  
Balance iron

with impurities due to melting.

7. A pre-alloy powder as claimed in any one of Claims 1 to 3, consisting of by weight:—

20—25% Molybdenum  
20—25% Vanadium with or without Niobium  
20—25% Manganese  
Up to 7% Carbon  
Balance iron

with impurities due to melting.

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